



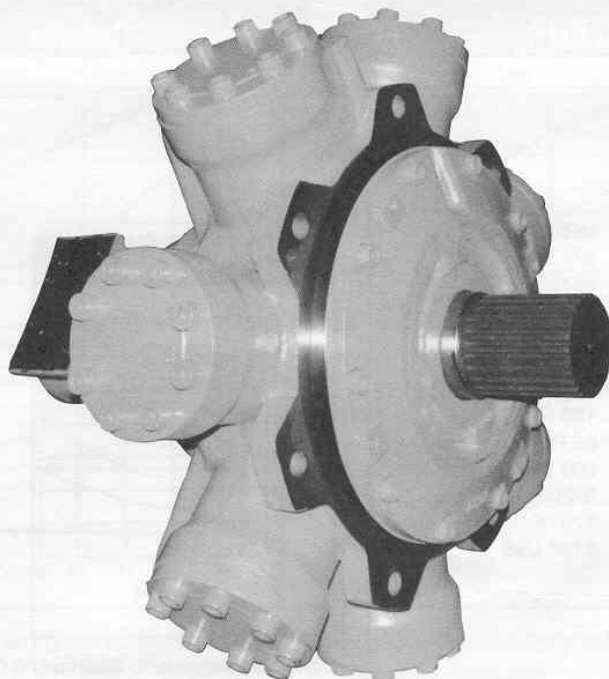
# **MRH-375**

# **MRH2-375**

Low Speed – High Torque

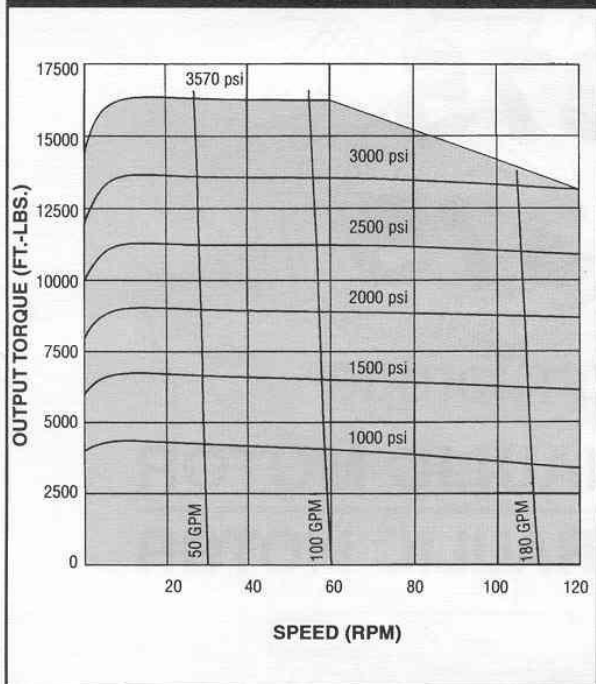
**SINGLE SPEED HYDRAULIC MOTOR**

**MULTIPLE SPEED HYDRAULIC MOTOR**



**KYB®**

## MRH-375 Performance Curve



## SPECIFICATIONS

### DISPLACEMENT:

MAX. CONT. PRESSURE:

INTER. PEAK PRESSURE:

MAX. BACK PRESSURE:

MAX. CONT. OUTPUT TORQUE:

MIN. STARTING TORQUE

MAX. CONT. SPEED @ 3000 PSI:

MAX. CONT. SPEED @ 3570 PSI:

MAX. CONT. POWER:

MOMENT OF INERTIA (GD<sup>2</sup>):

MAX FLUID TEMP:

DRY WEIGHT:

MRH-375-SW

377.5 IN.<sup>3</sup>/REV

3570 PSI

4000 PSI

350 PSI

16300 FT-LBS

12700 FT-LBS

120 RPM

60 RPM

300 HP

9820 LB-IN<sup>2</sup>

175 °F

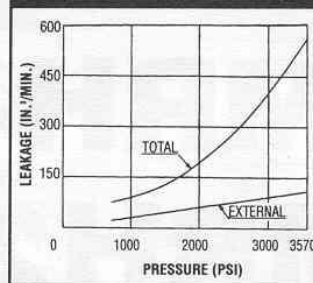
1150 LBS

## HOW TO ORDER

Model	Displacement	Shaft Type	Ports
MRH	— 375	— S	W

## Graph 1

### Static Leakage

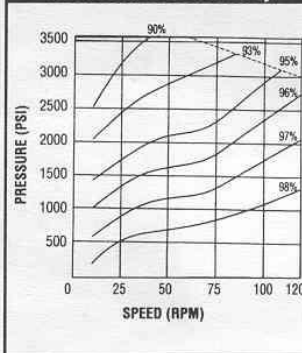


**Total static leakage is: internal leakage & external leakage.** Total static leakage is used when the outlet port is blacked and the torque load attempts to rotate the shaft as in winch applications. Values given will be considerably greater unless sufficient inlet pressure is maintained. The creep speed can be calculated from the following formula:

$$\text{Creep Speed (RPM)} = \frac{\text{Total Static Leakage (IN.<sup>3</sup>/MIN.)}}{377.5 \text{ (IN.<sup>3</sup>/REV.)}}$$

## Graph 3

### Volumetric Efficiency



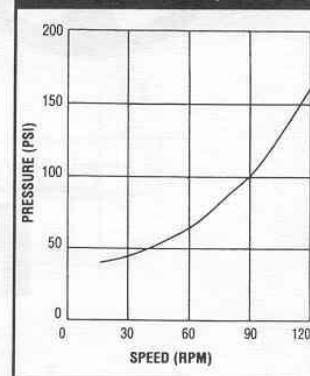
Input flow required to attain any given speed and pressure can be calculated from the graph using the nominal motor displacement of 377.5 cu. in./rev.

$$\text{Input Flow (IN.<sup>3</sup>/MIN.)} = \frac{377.5 \text{ (IN.<sup>3</sup>/REV.)} \times \text{Motor Speed (RPM)} \times 100}{\text{Motor Volumetric Efficiency (\%)}}$$

1 GAL./MIN. = 231 IN.<sup>3</sup>/MIN.

## Graph 2

### Idling Pressure Requirement



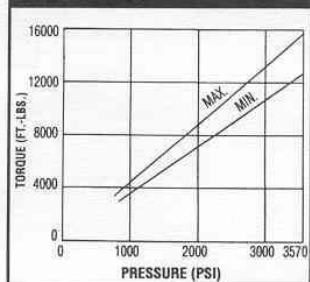
Graph 2 indicates pressure difference required to idle the motor at various speeds and no output torque. Values will be slightly greater at higher viscosities.

Caution should be taken to assure sufficient inlet pressure is maintained to prevent cavitation when the motor operates as a pump or when the load overruns the motor. Sufficient back pressure should be maintained to counteract centrifugal forces in the motor. Back or boost pressure is the pressure present at the low pressure port of the motor. These minimum pressures can be calculated as follows:

$$\text{Boost or Back Pressure (PSI)} = \frac{1}{2} \text{ Idling Pressure (PSI)} + \text{Crankcase Pressure (PSI)}$$

## Graph 4

### Starting Torque Characteristic



Starting torque varies with the crankshaft angle and maximum and minimum values are shown by the graph. A reduction in torque occurs if back pressure is excessive but viscosity effects are negligible.

Above curves are results obtained on mineral oil of 160-200 SUS viscosity.

OIL AND FILTRATION

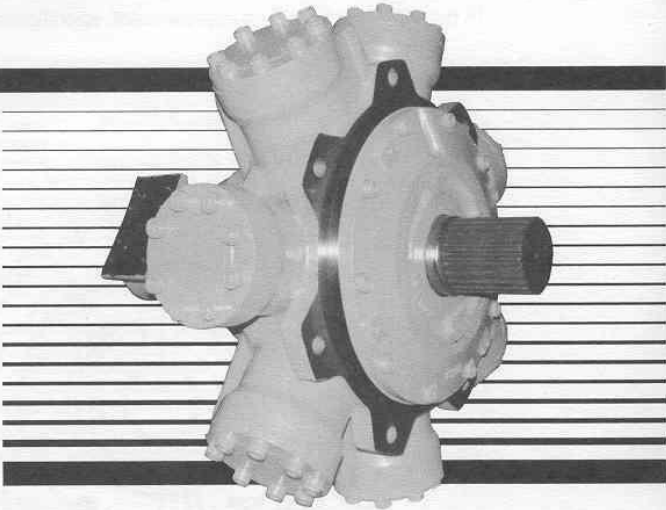
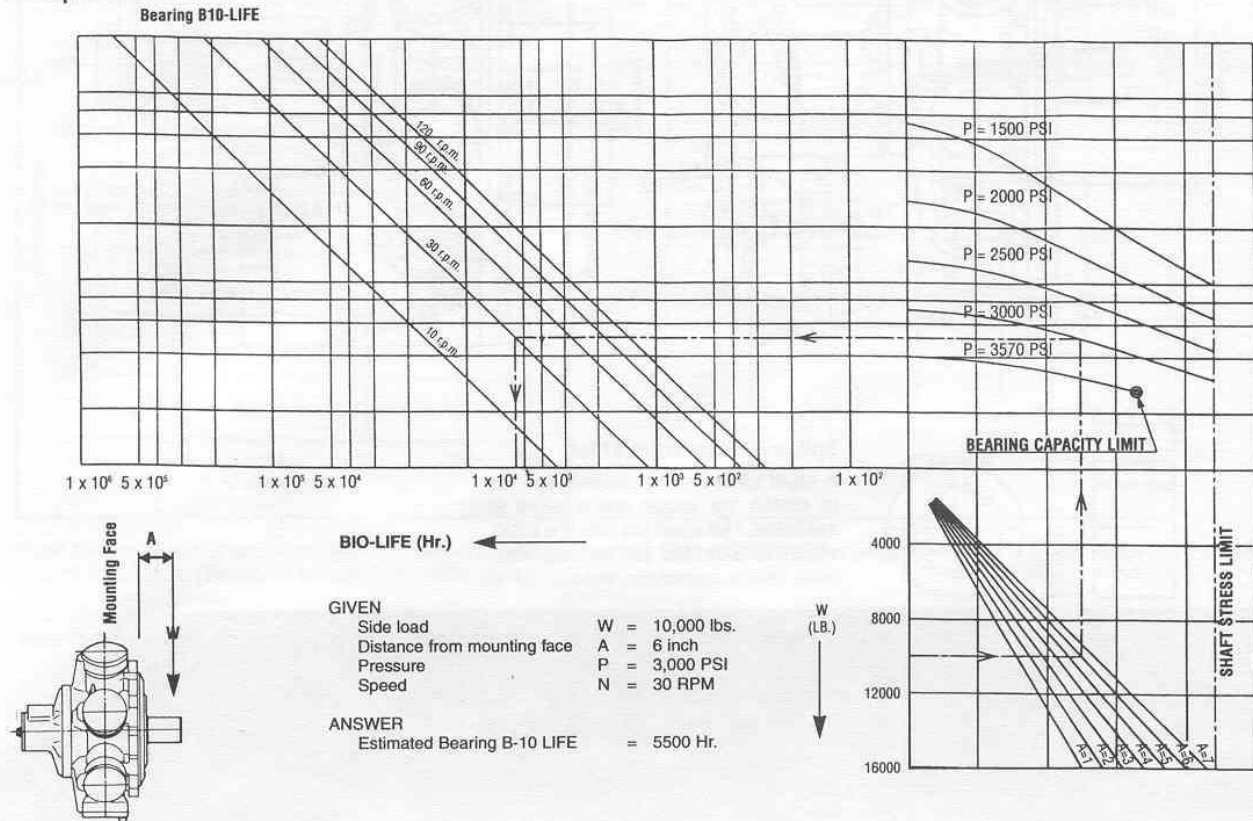
Because the oil not only transfers the force but also lubricates mating parts of the motor, care must be taken to assure minimum fluid viscosity is 120 SUS. However, it is recommendable for continuous operation to maintain the viscosity between 165 and 345. Maximum operating temperature should be less than 175°F.

However, even when the proper oil is used, wear will accelerate as oil becomes contaminated. The hydraulic fluid's life depends on conditions under which it is used and only experience can determine precise intervals at which fluid should be changed. With mineral oils it is recommended that samples be taken at about 1000 hour intervals and sent to the manufacturer for analysis. This will help determine the best timing for fluid changes. Filtration recommendation is 25 micron. Generally the pumps are more critical to contamination, therefore, it is advisable to investigate what filtration will be required to sustain the life of the pump.

BEARING B10-LIFE

Bearing B10-LIFE of taper roller bearings used in HYDROSTAR motors is explained in Graph 5 below. Bearing B10-LIFE is the number of hours at which 10% of the bearings may be expected to show some evidence of wear. The other 90% will be satisfactory. In fact, the average life of the bearings is 4 times the B10-LIFE.

Graph 5

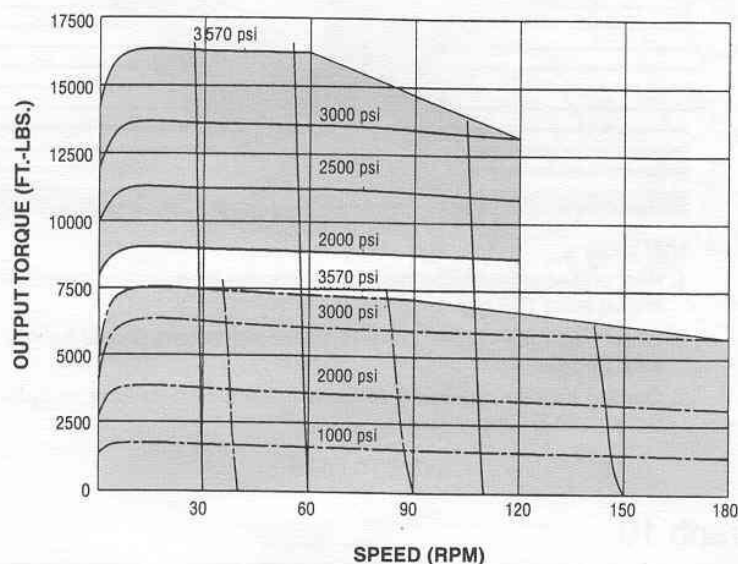


MINIMUM OPERATING SPEED

Minimum operating speed of 1 rpm is possible depending on load characteristics, but smooth performance of 3 rpm is normal. Starting torque varies with crankshaft angle. A reduction in torque occurs if the back pressure is excessive, but viscosity effects are negligible.

# MRH2-375 Multiple Speed Hydraulic Motor

## MRH2-375 Performance Curve



## SPECIFICATIONS

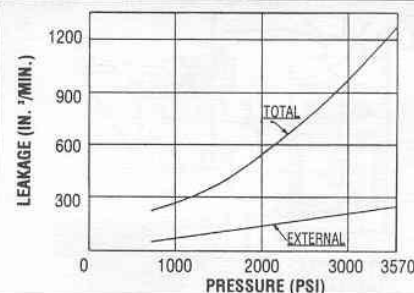
DISPLACEMENT (IN. <sup>3</sup> /REV):	MRH2-375-1 377.5 / 188.7	MRH2-375-2 377.5 / 0
MAX. CONT. PRESSURE (PSI):	3570	3570 / 150
INTER. PEAK PRESSURE (PSI):	4000	4000 / 250
MAX. BACK PRESSURE (PSI):	350	350 / -
MAX. CONT. OUTPUT TORQUE (FT.-LBS.):	16300 / 7450	16300 / 0
MAX. CONT. SPEED (RPM) @ 3000 PSI:	120 / 180	120 / -
MAX. CONT. SPEED (RPM) @ 3570 PSI:	60 / 90	60 / -
MAX. CONT. POWER (HP):	300	
MOMENT OF INERTIA (GD <sup>2</sup> ) (LB-IN <sup>2</sup> ):	9820	
MAX FLUID TEMP (°F):	175	
DRY WEIGHT (LBS):	1200	

## HOW TO ORDER

Model	No. of Speeds	Displacement	Shaft Type	Ports
MRH	2 — 375 —	<input type="checkbox"/>	— S	W
		See specification chart for displacement designation	(Standard)	SAE 4-bolt Flange

Graph 6

## Static Leakage

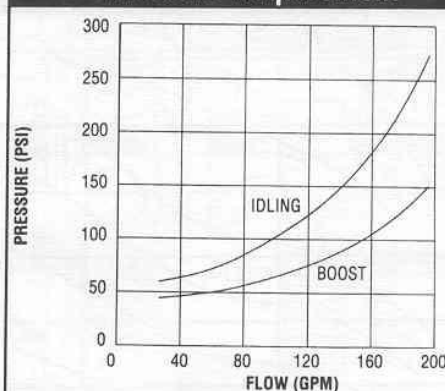


Total static leakage is the combination of internal leakage and external leakage. Total static leakage is used when the outlet port is blocked and the torque load attempts to rotate the shaft, such as a winch application. Unless significant back pressure is maintained, the creep speed will increase drastically and the motor may rotate out of control. The creep speed can be calculated from the following formula:

$$\text{Creep Speed (RPM)} = \frac{\text{Total Static Leakage (IN.<sup>3</sup>/MIN.)}}{377.5 \text{ or } 188.7 \text{ (IN.<sup>3</sup>/REV.)}}$$

Graph 7

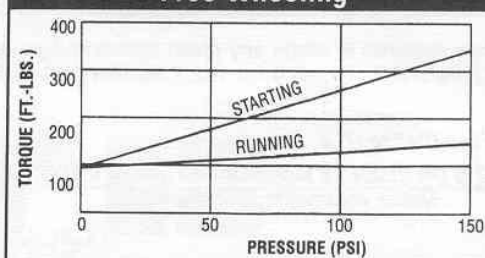
## Idling Pressure and Boost Pressure Requirement



Boost or Back Pressure (PSI) = 1/2 Idling Pressure (PSI) + Crankcase Pressure (PSI)

Graph 8

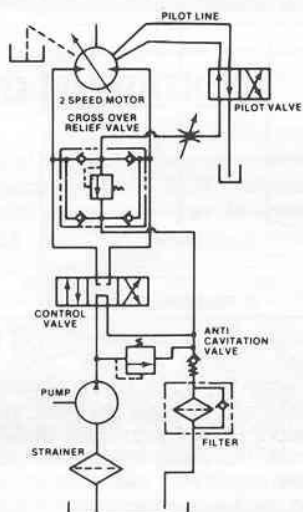
## Torque Requirement When Free Wheeling



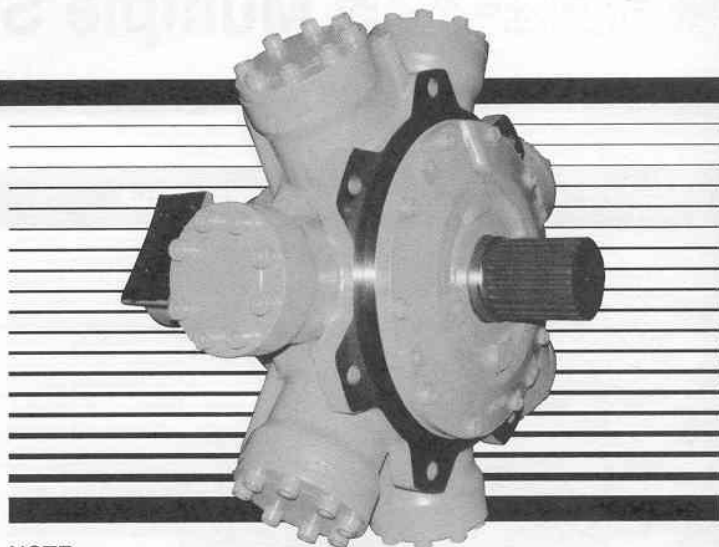
Input torque to motor when free wheeling.



## TYPICAL CIRCUIT



TWO SPEED MOTOR

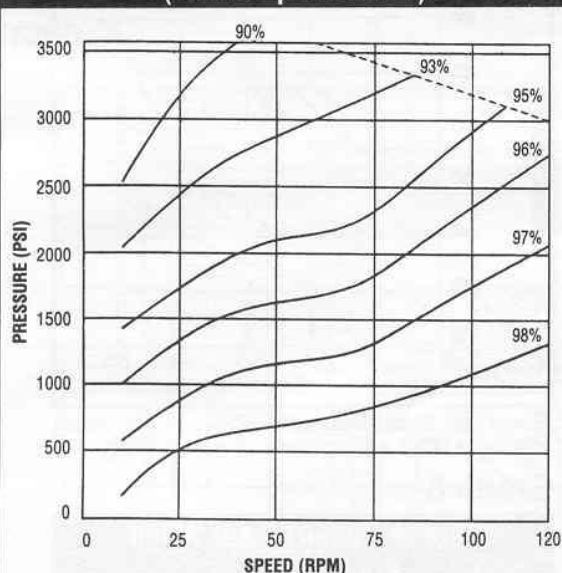


### NOTE:

1. Pilot pressure should be equal to or greater than system pressure and at least 150 psi.
2. When freewheeling the pressure above the pistons should be less than 200 psi.
3. Cooling may be required if motor is freewheeled for long periods. Consult KYB Corp.

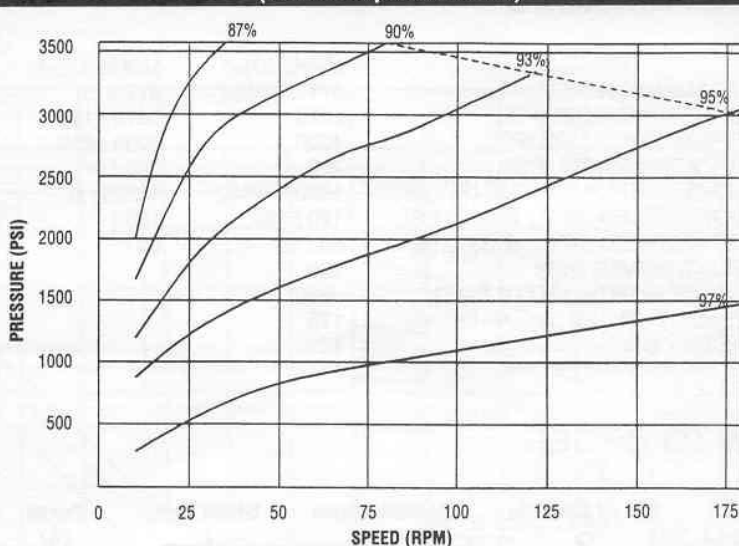
Graph 9

### Volumetric Efficiency (Full Displacement)



Graph 10

### Volumetric Efficiency (Half Displacement)



Input flow required to attain any given speed and pressure can be calculated from the graph using the nominal motor displacement of 377.5 IN.<sup>3</sup>/REV. (Graph 9) or 188.7 IN.<sup>3</sup>/REV. (Graph 10).

Input Flow (IN.<sup>3</sup>/MIN) =

$$\frac{377.5 \text{ (IN.<sup>3</sup>/REV.)} \times \text{Motor Speed (RPM)} \times 100}{\text{Motor Volumetric Efficiency (\%)}}$$

OR

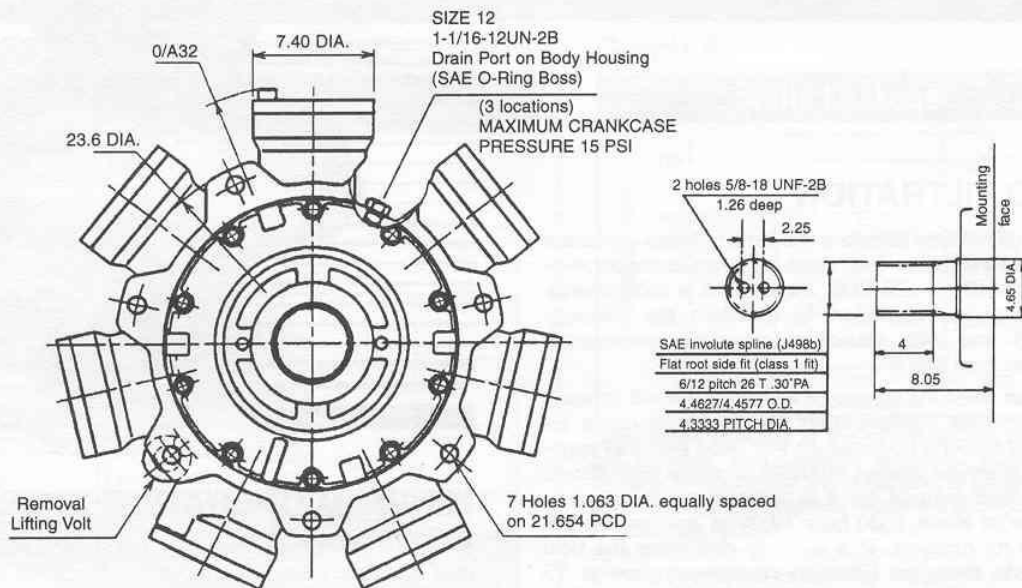
$$\frac{188.7 \text{ (IN.<sup>3</sup>/REV.)} \times \text{Motor Speed (RPM)} \times 100}{\text{Motor Volumetric Efficiency (\%)}}$$

$$1 \text{ GAL./MIN.} = 231 \text{ IN.<sup>3</sup>/MIN.}$$

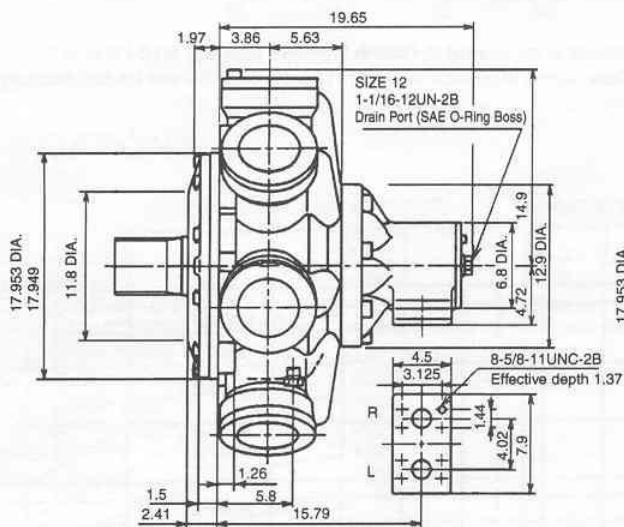
Above curves are results obtained on mineral oil of 160-200 SUS viscosity.

# MRH-375 & MRH2-375 Installation Dimensions

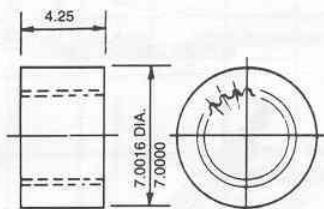
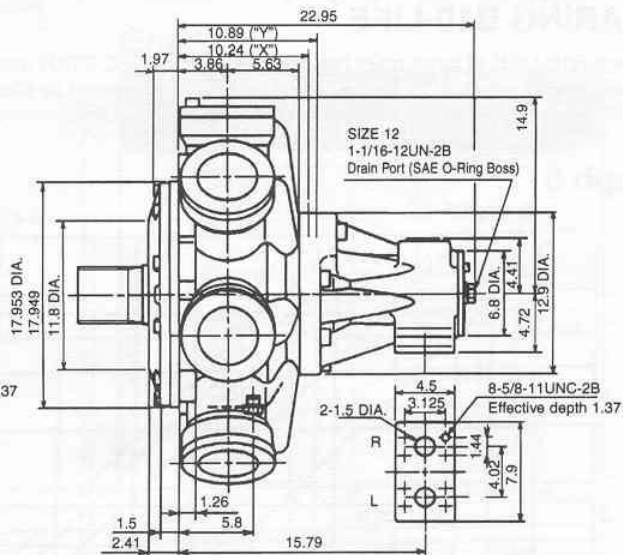
In the interest of product improvement, specifications and dimensions are subject to change without notice.



MRH-375-SW



MRH2-375-SW



## Spline adapter billet 37520

A steel billet having internal splines to match the motor spline shaft is available. The shaft fits into the billet, which is intended for welding onto drive gears, sprockets, etc.



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